

Corrosion prevention is an essential factor in the economic utilisation of steel. Provision of the appropriate protective coating can bring initial savings plus substantial economics in service, due to reduction or elimination of maintenance and lost service time, and by deferring the replacement date of structures and equipment. In suitable applications hot dip galvanizing provides ideal corrosion protection for steel - no other coating quality, durability, predictable performance, low maintenance, and resistance to abrasion and mechanical damage.

# INTRODUCTION

When designing a structure which is to be hot dip galvanized, it must be borne in mind that articles Edges are immersed into and withdrawn from a bath of molten zinc heated to a temperature of about 450°C. Design and fabrication is required to conform to acceptable standards which apply, regardless of whether a galvanized or a painted coating is to be applied. In the case of galvanizing, some additional requirements which aid access and drainage of molten zinc, will improve the quality of the coating and also reduce costs

With certain fabrications, holes which are present for other purposes may fulfil the requirements of venting of air and draining of zinc; in other cases it may be necessary to provide extra holes for this

For complete protection, molten zinc must be able to flow freely to all parts of the surfaces of a fabrication. With hollow sections or where there are internal compartments, the galvanizing of the internal welding is preferred since this method does not result in the presence of tightly adhering surfaces eliminates any danger of hidden corrosion occurring in service.

#### Some general principles for guidance are: • Holes both for venting and draining should be as large as possible. The absolute minimum

- hole sizes are given in table 2 Holes for venting and draining should be diagonally opposite one another at the high
- point and low point of the fabrication as it is suspended for galvanizing (figure 10).
- With hollow sections sealed at the ends, holes should be provided, again diagonally op-Punching posite one another, as near as possible to the ends of the hollow member (figure 8). In some cases it may be more economical to provide "V" or "U" shaped notches (figure 9) in the ends of the tubes, or to grind corners off rectangular hollow sections. These procedures will provide ideal means for venting and draining.
- Where holes are provided in end plates or capping pieces, they should be placed diagonally opposite to one another, off centre and as near as possible to the wall of the member to which the end plate is connected (figure 7).
- Internal and external stiffeners, baffles, diaphragms, gussets etc., should have the corners generously cropped with centre holes (particularly for "Road Sign Gantry" type of configurations) to aid the flow of molten zinc and to prevent air entrapment (figures 2, 11 and 24 and detail X).
- Bolted joints are best made after hot dip galvanizing.

Facilities exist to galvanize articles of virtually any size and shape (see list of members with kettle sizes - available from the Hot Dip Galvanizers Association). When an article is too big for single immersion in the largest bath available it may be possible to galvanize it by double-end dipping Shearing and Flame Cutting (table 1), depending on the handling facilities and layout of the galvanizing plant (check with the galvanizer). Large cylindrical objects can often be galvanized by progressive dipping (figure 1).

#### MODULAR DESIGN

Large structures are also hot dip galvanized by designing in modules for later assembly by bolting or welding. Modular design techniques often produce economics in manufacture and assembly through simplified handling and transport (see also Masking).

**STEEL GRADE** 

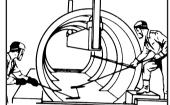
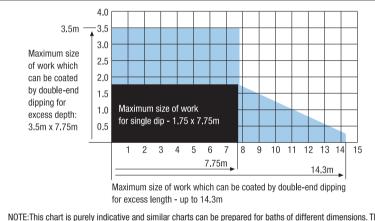


Figure 1

It is possible to hot dip galvanize all structural steels and the ultimate coating thickness achieved is determined by steel analysis, immersion time and to a lesser degree, zinc temperature. In modern stee making practice, either aluminium or silicon is added to molten steel as de-oxidising agents. Aluminium ad-



NOTE: This chart is purely indicative and similar charts can be prepared for baths of different dimensions. The maximum sizes which a particular galvanizer can process should always be checked at the design stage. Table 1

ditions (as in aluminium-killed steel - Si less than 0.04%) has no effect on the structure and coating thickness. Silicon-killed steel with silicon (Si) ranging between 0.15 to 0.25% is ideal for heavy duty coatings. On either side of this range, excessively thick and brittle coatings can Zinc Rich Epoxy or Zinc Rich Paint develop if extended immersion times in molten zinc cannot be avoided. The immersion cycle is determined by the configuration of the structure and thickness of the section. (The thicker the steel, the longer the immersion time). The impact of phosphorous (P) in steel can be severe regardless of the Si present. At levels below 0.015% P has little influence on coating growth. Above 0.02% the effect is extremely severe even when Aluminium-killed steel is galvanized. It is for faces are to be properly dried. this reason that hot dip galvanizing specifications provide for minimum coating thickness and no maximum limit is set. The specification does not stipulate a maximum upper coating A zinc rich paint or epoxy containing greater than 80% zinc in the dry film, should be applied to thickness. (See NOTE 1 in "Specifying Hot Dip Galvanizing").

### BENDING AND FORMING AFTER HOT DIP GALVANIZING

Components which have been hot dip galvanized should not be bent or formed by applying heat above the melting temperature of zinc as this can cause embrittlement due to intergranular liquid zinc penetration between steel crystal boundaries.

#### **FABRICATION DEFECTS**

be removed prior to galvanizing

Burrs

Unlike a paint coating, burrs will be overcoated by hot dip galvanizing but the removal of a burr after Products are now available in a two component, solvent free form, packed for convenience in galvanizing may result in the presence of a small uncoated surface and for this reason, burrs must handy, easy to use squish packs. One of these products is available from the Association and all

GUIDELINES FOR MINIMUM VENT AND E HOLE SIZES - REQUIRED BY SECTION LENGTH Tube Dia ≤ 50 60 - 76 89 102 - 114 127 - 152 165 219 245 273 324 355 80 x 40 80 x 80 90 x 90 200 x 100 180 x 180 200 x 200 300 x 200 400 x 200 300 x 300 RHS Sizes 50 x 30 160 x 80 60 x 40 70 x 70 120 x 60 120 x 80 120 x 120 150 x 150 250 x 150 220 x 220 250 x 250 450 x 250 (mm) 50 x 50 100 x 50 100 x 100 150 x 100 340 x 200 60 x 60 76 x 76 140 x 140 Length (m) Hole size (mm) 10 (12) 10 (12) 12 (2x10) **16** (2x12) **20** (2x16) **25** (2x20) **30** (2x25) **30** (2x25) **40** (2x30) **40** (2x30) 10 (12) 10 (12) 12 (2x10) 12 (2x10) 16 (2x12) 20 (2x16) 25 (2x20) 30 (2x25) 30 (2x25) 40 (2x30) 50 (2x40) 10 (12) 10(12) 12 (2x10) 12 (2x10) 12 (2x10) 16 (2x12) 20 (2x16) 25 (2x20) 30 (2x25) 40(2x30)50 (2x40) 50 (2x40) 12 (2x10) 12 (2x10) 16 (2x12) 16 (2x12) 16(2x12)25 (2x20) 25 (2x20) 30(2x25)40(2x30)50 (2x40) 2x50 (3x40 12 (2x10) 16 (2x12) 16 (2x12) 16 (2x12) 25 (2x20) 25 (2x20) 30 (2x25) 30 (2x25) 50 (2x40) 50 (2x40) 2x50 (3x40 2x50 (3x40) 2x50 (3x40 12 (2x10) 16 (2x12) 20 (2x16) 20 (2x16) 25 (2x20) 25 (2x20) 50 (2x30) 50 (2x40) 50 (2x40) 16(2x12)16 (2x12) 20 (2x16) 20 (2x16) 25 (2x20) 25 (2x20) 50 (2x30) 50 (2x40) 50 (2x40) 2x50 (3x40) 2x50 (3x40 16 (2x12) 16 (2x12) 20 (2x16) 25 (2x20) 25 (2x20) 2x25 (3x20) 50 (2x30) 50 (2x40) 2x50 (3x40) 2x50 (3x40) 2x50 (3x40) 16(2x12) 16 (2x12) 25 (2x20) 25 (2x20) 2x25 (3x20) 2x25 (3x20) 50 (2x30) 2x50 (3x40) 2x50 (3x40) 2x50 (3x40) 2x50 (3x40) 9 10 +20 (2x16) 25 (2x16) 25 (2x20) 25 (2x20) 2x25 (3x20) 2x25 (3x20) 50 (2x30) 2x50 (3x40) 2x50 (3x40) 2x50 (3x40) 2x50 (3x40) Note: The hole sizes specified above may be substituted with a larger number of smaller holes. (minimum ø 10mm for vent and ø 12mm for fill/drain hole)

Table 2

# RELIABILITY

The hot dip galvanized coating is formed by a metallurgical reaction between suitably cleaned steel and molten zinc. This results in the Ease of inspection and dependability in service are beneficial features of a hot dip galvanized coating. The cathodic protection of steel by formation of a series of iron/zinc alloys which are overcoated with relatively pure zinc. The process entails total immersion of components in zinc ensures that corrosion of the underlying steel cannot occur as long as zinc is present. Even at discontinuities on the coating, both pretreatment chemicals and molten zinc. This ensures uniform protection and coating reliability even on surfaces which would be corrosion creep under the surrounding zinc is not possible. inaccessible for coating by other methods.

Because a hot dip galvanized coating is formed by metallurgical reaction between molten zinc and steel, the coating thickness on edges and corners is equal to, or thicker than that on flat surfaces. Thus the rounding of sharp edges, as required for paint coatings, is not necessary. If subsequent painting is required, sharp edges should be rounded during fabrication to a radius of 3mm or 50% of steel thickness.

Welds should be continuous and free from excessive pin-holing and porosity. Weld slag, normally associated with stick welding, is not readily removed by acid cleaning and such slag must be removed by mechanical means prior to hot dip galvanizing. Shielded arc

#### Weld Spatte

Weld spatter does not reduce the protective properties of a hot dip galvanized coating to the same extent as a paint coating, but it is recommended practice to remove spatter prior to hot dip galvanizing.

Full size punching of holes is permitted when (amongst other requirements such as distortion free, burr free, not subject to fatigue), according to Clause 4.3.6.3.c of SANS 2001-CS1, "the thickness of the material is not greater than the hole diameter plus 3mm; nor greater than

Clause 4.3.6.4 Punching and reaming reads: "Punching is permitted without the conditions of 4.3.6.3 provided the holes are punched at least 2mm less in diameter than the required size and the hole is subsequently reamed to the full diameter."

Material of any thickness may be punched at least 3mm undersize and then reamed, or be drilled. Good shop practice in relation to ratios of punched hole diameter to plate thickness, and

punch/die diametral clearance to plate thickness should be observed. For static loading, holes may be punched full size in material up to  $\frac{4500}{-}$  mm thick where Fy is material vield stress up to 360MPa

Edges of steel sections greater than 16mm thick subject to tensile loads should be machined or machine flame cut. Edges of sections up to 16mm thick may be cut by shearing.

Sheared edges to be bent during fabrication should have stress raising features such as burrs and flame gouges removed to a depth of at least 1.5mm. Temperatures associated with flame cutting alter the surface properties of steel and if such surfaces are not thoroughly ground, a thinner galvanized coating will be formed (usually below the minimum **specified).** Before bending, edges should be radiused over the full arc of the bend.

Steels that are susceptible to embrittlement and fatigue failure should be bent over a smooth mandrel with a minimum radius 2 to 3 times material thickness. Where possible hot work at red heat. Cold bending is unlikely to affect steels less than 3mm thick.

### **COATING REPAIR PROCEDURES**

#### By the Galvanize

In terms of SANS 121:2011 (ISO 1461:2009) a galvanizer may repair a coating by either zinc metal spraying or zinc rich epoxy. The latter method must conform to certain requirements in the specification. The preferred method of repair is by zinc metal spraving. Repair will only be necessary if bare spots are present, usually caused by inadequate cleaning, air entrapment or if mechanical damage has occurred.

No single uncoated area shall exceed 10cm<sup>2</sup> and the total uncoated areas for renovation by the galvanizer or on site shall not exceed 0.5% of the total area of the component.

#### Zinc Metal Sprayed Coatings Method

The damaged area is to be lightly blasted using preferably a pencil blasting nozzle or the surrounding coating should be masked in order to limit damage.

A zinc metal sprayed coating is then applied to the abrasive blasted surface to a 100µm thickness or equal to the surrounding coating thickness, if a duplex coating is to be applied. The repaired area is then wire brushed, (preferably stainless steel) to remove loosely adhering over sprayed zinc.Wire brushing provides the added benefit of sealing the pores that may be present in the spraved coating

**Coating Repair Products** 

of its members.

The preferred product is a two component zinc rich epoxy.

Method

The defective area shall be blasted as above or abraded with abrasive paper (roughness 80 grit). All dust and debris must be completely removed. In the event of moisture being present, all sur-

a DFT of 100µm (overlapping the bare spot by 5mm) or equal to the surrounding coating thickness, if a duplex coating is to be applied

Approved products for repair were only available in large containers. Due to the large quantities

involved and short pot life when mixed, the products proved to be expensive and wasteful.

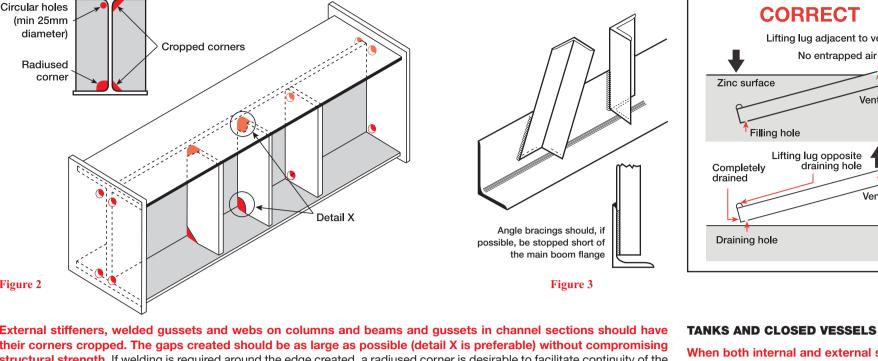
To ensure compliance in all aspects of the standard, specifiers nd customers on enquiry should request a certificate of conormance to ISO10474 such as the SABS Mark Scheme. For echnical support from the HDGASA a member of the Associaion, is preferred.

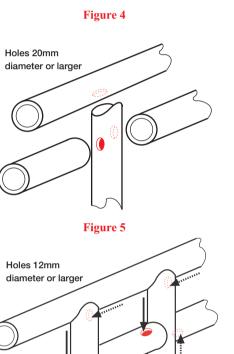
When hot dip galvanizing is specified, the surface of the base steel is completely covered with a relatively uniform coating of zinc and the minimum thickness specified is related to the thickness of the steel being hot dip galvanized, as shown in table 3.

### HOT DIP GALVANIZING SPECIFICATIONS

fications and test methods. SANS32 (EN10240:1997): Internal and/or external protective

coatings for steel tubes - Specificaapplied in automatic plants.

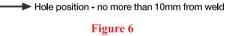




**Figure 6** 

Open mitred joint





## **VENTING, FILLING AND DRAINAGE**

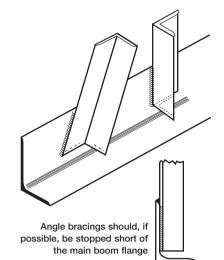
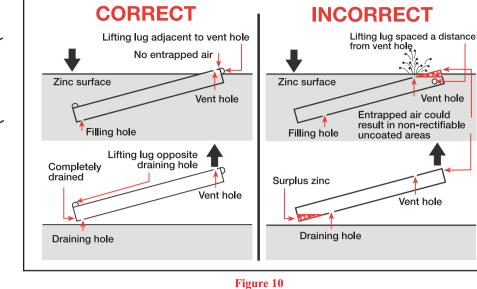


Figure 3



When both internal and external surfaces are to be hot dip galvanized at least one

structural strength. If welding is required around the edge created, a radiused corner is desirable to facilitate continuity of the weld around the cut end to the other side. Circular holes are less effective: if used, they should be as close to corners and edges as practicable. Where more convenient, the cropped corners or holes may be in the main beam. Consultation with the galvanizer, regarding the appropriate vent and drainage hole sizes is recommended.

### WELDED PIPE SECTIONS

Closed sections must never be incorporated in a fabrication. Sections should Internal baffles should be cropped as illusbe interconnected using open mitred joints as illustrated in figure 4, or intercon- trated or as per detail X above, especially for necting holes should be drilled before fabrication as in figure 5.

Alternatively external holes may be positioned as in figure 6, a method which holes in baffle plates and base plates. Manis often preferred by the galvanizer, since quick visual inspection shows that holes or pipes should finish flush inside to the work is safe to galvanize.

Pipe ends can be left open, or provided with removable plugs (see unwanted Lifting lugs should be provided opposite the vent holes).

#### **SMALL TUBULAR FABRICATIONS**

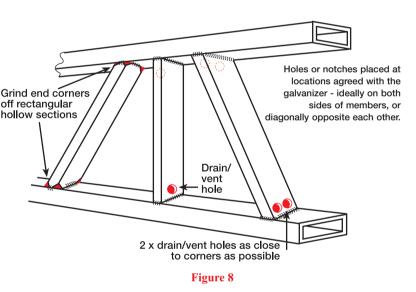
Small tubular fabrications must be vented, preferably with holes not less than 10mm diameter (see table 2)

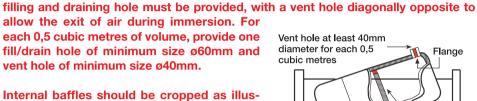
### **UNWANTED VENT HOLES**

These may be closed by hammering in lead plugs after galvanizing and filing off flush with surrounding surfaces.

#### **TUBULAR FABRICATIONS/HOLLOW STRUCTURALS**

Drain/vent hole sizes should be preferably 25% of internal diameter or diagonal dimension for sections yielding a maximum cross sectional area of 180cm<sup>2</sup>. This percentage can be dependent on the shape of the fabrication, therefore consultation with the galvanizer at the design stage is recommended. FOR MUCH IMPROVED COATING QUALITY, REDUCED COATING GROWTH, PROVIDING AN IMPROVED AESTHETICALLY PLEASING AP-ATELY SIZED AND POSITIONED FILL. DRAIN AN VENT HOLES CAN MAKE A HUGE CONTRIBUTION.

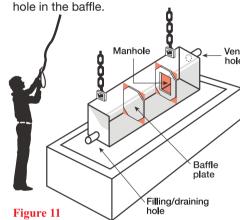




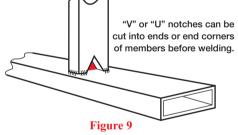
structures such as "Road Sign Gantries" which also require considerably larger centre prevent trapping excess zinc.

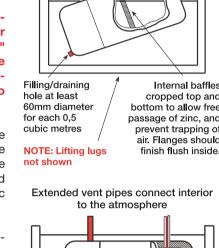
biggest and most accessible filling / draining hole NOTE: Lifting lugs and adjacent to the vent hole on the opposite not shown end (see figure 10). The lugs must be designed to accommodate the excess mass of molten zinc Extended vent pipes connect interior within the cylinder / pipe on withdrawal.

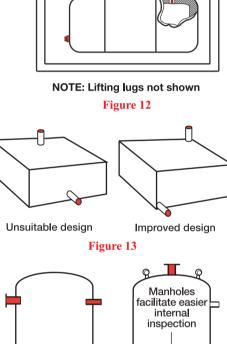
Large vessels require an appropriate size man-



When vessels and heat exchangers etc., are not to be galvanized inside. 'snorkel' tubes or extended vent pipes must be fitted after discussion with the galvanizer, to allow air to exit above the level of molten zinc in the galvanizing bath.







Remaining

Unsuitable design

Figure 14

Finish pipe or manhole flush with inside of vesse Improved design

abricated assemblies, castings and other components for hot dip galvanizing should be inspected and any significant surfaces lentified, before despatch to the galvanizer to ensure that the following points conform to design requirements. This may avoid costly rectification and delays at the galvanizing plant.

### SIZE AND SHAPI

MASKING

WELD SLAG

castings.

alvanized

DISTORTION

Distortion can be minimised by:

Use of symmetrical designs

to minimise stresses.

mising their positions.

water quenching.

Thin sheets

Figure 16

the Association for further information.

**COMBINATIONS OF FERROUS SURFACES** 

be abrasive blast cleaned before galvanizing.

leld slag must be removed by abrasive blast

leaning, de-scaling, chipping, grinding,

lame cleaning or a pneumatic needle gun.

PROVISION FOR HANDLING

abrications containing a combination of castings

and steels, or rusted and mill scaled surfaces must Remove weld slag

sheet to prevent the penetration of acid into any conceivable crevice.

**MATERIALS SUITABLE FOR HOT DIP GALVANIZING** 

oldered or aluminium rivetted cannot be hot dip

ticularly when steel is less than 3 - 4mm thick.

mum bend radius to minimise stress.

vent distortion during hot dip galvanizing.

All ferrous materials are suitable, including sound stress-free

In case of double-sided fillet welds, the weld must be continued around the ends of the

Check that work is suitably sized and dimensioned for the handling and galvanizing facilities of the selected galvanizer. It may be too late to make changes to the design but it is costly to despatch work which the galvanizer cannot process.

STRUCTURAL STEEL Check that punching, shearing and bending have been carried out in conformity with the recommendations above.

### SATISFACTORY HOT DIP GALVANIZING

- Check that welding slag and spatter have been completely removed (anti-spatter agents are highly recommended). Check that assemblies comprising castings and steels of widely differing surface conditions have been abrasive blast cleaned. This will minimise differences in the coating.
- Check that castings are abrasive blast cleaned before despatch unless otherwise arranged.
- Check that large grey iron castings have been normalised.
- markings (if necessary) have been provided.
- Check that an appropriate marking pen which is easily removed, has been used. Contact the Association.

DEPENDABILITY

THE ASSOCIATION IS A TECHNICAL INFORMATION CENTRE ESTABLISHED FOR THE BENEFIT OF SPECIFIERS, CONSULTING ENGINEERS, END USERS AND ITS MEMBERS JOHANNESBURG: Quality House, Unit U4, St. Christopher Road, St. Andrews, Bedfordview P.O. Box 2212 Edenvale 1610 Telephone: 011 454 6304 Email: hdgasa@icon.co.za • CAPE TOWN: Telephone: 021 797 4735 Email: terry@hdgasa.org.za • Website: www.hdgasa.org.za



The active for a set of the set o	04N04 4740 (1004 4740 0000)	Design of the second					
The galvanizer acts as a sub-contractor to a steel fabricator and as such, his contractual relationship is normally with the fabricator, not with the ultimate user or specifier. It is important, therefore, that	SANS14713 (ISU14713:2009)	<ul> <li>Protection against corrosion of iron and steel in structures - Zinc and alu- minium coatings - Guidelines.</li> </ul>	MINIM		ESS ON ARTICLES TH 121:2011 (ISO 1461)	IAT ARE NOT CENRIF 2009)	JGED —
the users' or specifiers' requirements for hot dip galvanizing are made clear to the fabricator and that all instructions are	SANS4998 (ISO4998:2005):	Continuous hot dip zinc coated carbon steel sheet of structural quality.	Profiles	Local coating thickness min. µm*	Local coating mass (minimum)	Mean coating thickness, min. μm*	Mean coating mass (minimum)
channelled (in writing) via the fabricator to the galvanizer. Al- ternatively, the selected galvanizer should be invited to partici-	SANS3575 (IS03575:2005):	5/5 (ISO3575:2005): Continuous hot dip zinc coated carbon steel sheet of commercial, lock form- ing and drawing grades.	Steel > 6mm	70	505	85	610
pate in the initial project team meetings, when surface finishes	( , , , , , , , , , , , , , , , , , , ,		Steel $>$ 3mm to $\leq$ 6mm	55	395	70	505
as in duplex coatings or "Architectural Hot Dip Galvanizing", are crucial.	BS EN ISO 10684:2004		Steel $\geq$ 1.5mm to $\leq$ 3mm	45	325	55	395
			Steel < 1.5mm	35	250	45	325
To ensure compliance in all aspects of the standard, specifiers					Table 3		

MINIMUM COATING THICKNESS ON ARTICLES THAT ARE CENTRIFUGED TO SANS 121:2011 (ISO 1461:2009)							
Diameter of the article	Local coating thickness min, um*	Local coating mass (minimum)	Mean coating thickness min, um*	Mean coating mass (minimum)			
> 6mm diameter	40	285	50	360			
≤ 6mm	20	145	25	180			
Table 4							

ariance in coating thicknes A requirement for a thicker coating (25% greater than the standard in table 3 above, can be requested for components not centrifuged, without affecting specification conformity)

Where steel composition does not include moderate to high reactivity, thicker coatings are not always easily achieved

In the case of large contracts, the galvanizer should be involved at the programming stage with the fabricator and the end user. Hot dip galvanizing is normally the final process after fabrication and prior to delivery and erection. If sufficient time for galvanizing and inspection is not provided in the overall programme, costly delays may occur at the erection stage.

Note 1: Hot dip galvanizing specifications state the minimum ac ceptable coating thickness, established by a minimum of 5 individual readings per reference area. The thickness actually chieved, varies with steel composition and this can range from the minimum up to at least 50% greater. As life expectancy predictions are normally based on the minimum coating thickness, they are usually conservative

The specification does not stipulate a maximum upper coating thickness limitation, however, excessively thick coatings on threaded articles SANS121 (ISO1461:2009): Hot dip galvanized coatings on fabri- are undesirable. In order to ensure effective tensioning an approcated iron and steel articles - Speci- priately oversized nut must be screwed on to the bolt for quality assurance purposes, this applies particularly to high strength bolts.

### LEAD TIMES

tion for hot dip galvanized coatings As a general guide, most articles can be hot dip galvanized and returned to the fabricator within 7 days after receipt.

# WELDING, HANDLING, MASKING, IDENTIFICATION, MINIMIZING **DISTORTION AND CLEARANCE FOR MOVING PARTS**

### **OVERLAPPING SURFACES**

Masking materials have been developed, which if applied prior to hot dip galvanizing, will **A minimum gap of at least 2mm between plates, overlapping surfaces and back-to**prevent the formation of the galvanized coating on surfaces where it is not desired. Contact back angles and channels, must be provided (figure 21).

When small overlaps are unavoidable, seal edges by welding.

In circumstances where seal welding is not practical, a degree of temporary surface staining at crevices may be apparent after hot dip galvanizing and quenching. This is often incorrectly described as acid staining. Clean with a bristle brush and mild detergent if necessary. Crevices of this nature can be sealed after hot dip galvanizing with an appropriate sealant.

(figures 2 & 24)

STRENGTHENING GUSSETS AND WEBS

Welded strengthening gussets and webs on

columns and beams, and strengthening gussets

in members fabricated from channel or I-beam

sections should have corners cropped or holed

to prevent the entrapment of air in pockets and

corners allowing complete access of pickle

#### LARGER OVERLAPPING SURFACES

Figure 23

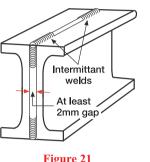
If contacting surfaces cannot be avoided, one diameter 10mm hole is to be provided in one of the members for every 100cm<sup>2</sup> of overlap area and the perimeter of the contacting area should be continuously welded (figure 23). A vent hole in Nork not suitable for handling with chains, baskets, hooks or jigs must be provided one member will ensure the safety of galvanizing personnel with suspension holes or lifting lugs (see figure 10). If in doubt check with the galva- and prevent damage to the article.

ø 10mm hole through one member

acids and molten zinc to the entire surface of the work, and

• to facilitate drainage during withdrawal from degreaser, acid

Minimum radial clearance



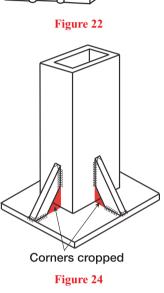


Figure 20

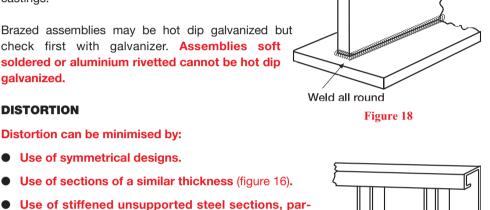
#### **OVERSIZE TAPPING ALLOWANCE FOR HOT DIP GALVANIZED NUTS**

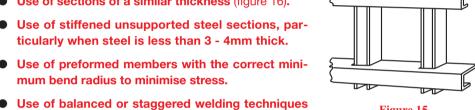
The zinc coating on external threads shall be free from lumps and shall not have been subjected to a cutting, rolling or finishing operation that could damage the zinc coating. The zinc coating of an external standard metric thread that has not n undercut shall be such : to enable the threaded part to fit an oversized tapped nut in accordance with the allowances given in the table below (See also NOTE 1 in "Specifying Hot

#### Nominal size Allowance of thread (mm)

16 to M24	0,38	
8 to M12	0,33	

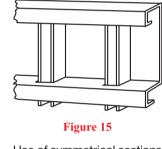
should be increased to 0,4mm.





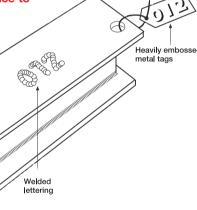
hot dip galvanizing. Avoid combinations of thick and thin materials. Bolt togethe after individually hot dip gal-

Air cooling after hot dip galvanizing in preference to



Use of symmetrical sections Large open fabrications, thin walled trough sections minimises distortion during and tanks may require temporary cross stays to pre-Maximising fill, drain and vent hole sizes and opti-

• Complete and rapid immersion of the item in the galvanizing bath, i.e no double end dipping.



### solutions, rinsewater, flux and molten zinc. **CLEARANCE FOR MOVING PARTS** Drop handles, hinges, shackles, shafts and spindles require a minimum radial clearance, to allow for the thickness of the hot dip galvanized coating (see below). Shaft or spindle size

Up to 30mm diameter Over 30mm diameter



### **IDENTIFICATION MARKINGS**

For permanent identification use heavily embossed, punched or welded lettering. For temporary identification use heavily embossed metal tags wired to the work, water soluble paint or the correct marking pen.

**Do not use enamel/oil paints, adhesive labels or any other coating that cannot be** On bolts greater than M24, unreadily removed by degreasing or pickling. If present, these coatings require to be re- dercutting of bolt threads is fremoved by paint stripper, grinder or abrasive blasting prior to pickling and hot dip gal- quently preferred to oversizing vanizing. An appropriate marking pen which is easily removable in the cleaning of nut threads. The allowance process is available (contact the Association).

**INSPECTION OF WORK BEFORE DESPATCH TO THE GALVANIZER** 

Figure 19

bservance of the points listed above will ensure optimum hot dip galvanized product quality and minimise extra costs or delays Check that closed vessels and tubular fabrications are vented with appropriate size holes, for safety and satisfactory hot dip gal

Check that all temporary fabrication markings are easily removed by the galvanizing process and that permanent identification

# THE HOT DIP GALVANIZERS ASSOCIATION OF SOUTHERN AFRICA

The Visio

The Hot Dip Galvanizers Association of Southern Africa was founded in 1965 and its membership represents the majority of the available hot dip galvanizing capacity of Southern Africa

#### prising all its Members and other interested parties, as a professional organization serving the interests of all parties dependant upon the hot

#### dip galvanizing industry. **Charter Statemen**

The primary role of the Hot Dip Galvanizers Association of Southern Africa is to promote a higher level of acceptance of, and confidence in, hot dip galvanized products and offerings on a national basis. The Association is the vehicle that provides all of its members with technical know-how and marketing support in order to grow the quality and acceptability of hot dip galvanizing in the marketplace.

The Hot Dip Galvanizers Association of Southern Africa is an advisory body and independent authority, representing the end-users, consumers 

HDGASA01-1990 Code of Practice for Surface Preparation and Apand specifiers of hot dip galvanized steel products, ensuring quality standards and customer satisfaction with the corrosion prevention system supplied by hot dip galvanizers of southern Africa.

**Delivery Activities** 

PREDICTABILITY

- Promoting the use of hot dip galvanizing for cost effective corrosion protection in applications where its use is appropriate. Providing technical assistance and advice for specifiers, fabricators
- and end users while also recommending alternative protective methods where appropriate.

- Participating in development projects on behalf of industry by providing assistance in the form of technical consulting, practical recommendations and assistance with the preparation of design specifications.
- Providing assistance with quality control during fabrication and hot dip galvanizing.
- To position the Hot Dip Galvanizers Association of Southern Africa, com- 

  Disseminating technical knowledge by providing a consulting and training service as well as the publication of technical literature. • Providing training and education for member companies to ensure
  - a high standard of quality and service throughout the galvanizing Publications Available from the Association
  - Association Magazine Hot Dip Galvanizing Today. (Free publication produced quarterly)
  - Steel Protection by Hot Dip Galvanizing and Duplex Coating Sys-
  - Practical Guidelines for the Inspection and Repair of Hot Dip Galvanized Coatings
  - plication of Organic Coatings Applied to New Unweathered Hot Dip Galvanized Steel. HDGASA02-1990 Specification for the Performance Requirements
  - of Duplex Coating Systems. HDGASA03-2006 Hot Dip Galvanizing and Duplex Coating Protec-
  - tion Specification. Hot Dip Galvanizing for Architectural Purposes Check List.
  - Wall Chart Design for Hot Dip Galvanizing.

Facts About Hot Dip Galvanizing

Identifying and investigating potential new applications for hot dip Please visit our website www.hdgasa.org.za for Information Sheets, Case Studies and other technical information.

The durability of a hot dip galvanized coating is determined by the degree of corrosion of zinc in a specific environment and the thickness of the coating. Corrosion of zinc is normally uniform, thus durability of a hot dip galvanized coating is predictable in most applications.

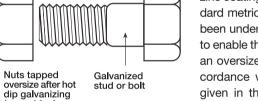


Figure 2

Figure 2

The galvanized coating on the bolt

Nuts tapped

no residua

des corrosion protection for ne internal thread on the nut.

Dip Galvanizing")